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**IMAGING AND/OR SCANNING APPARATUS WITH COMPENSATION OF
IMAGING DEGRADATIONS CAUSED BY THE SURROUNDINGS**

Description

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The invention relates to an imaging and/or raster-mode scanning apparatus and to a method for operating an apparatus of this type with a device for compensating for ambient influences that may cause imaging degradations.

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Imaging and/or raster-mode scanning apparatuses, for example scanning electron microscopes, force microscopes and light scanning microscopes, have attained great importance in many methods for inspecting samples.

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However, these measurements are frequently influenced by external ambient conditions such that the imaging quality is diminished. This results, under certain circumstances, in an undesirable degradation of the resolving power and/or in defective imaging. In the following text, an imaging degradation of this type is generally described as the occurrence of imaging or image defects. In the case of electron scanning microscopes, by way of example, an influencing variable that diminishes the imaging quality may be an electromagnetic interference field which influences the electron orbits. Furthermore, air and/or ground vibrations in the surroundings of the microscope are a factor for consideration, these causing losses of spatial definition in the illumination of the sample and/or in the detection of the electrons. The above-described influence of electromagnetic interference fields or air and/or ground vibrations on the imaging quality applies, in principle, to all imaging and/or raster-mode scanning apparatuses.

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One method for eliminating air and/or ground vibrations consists for example in putting the apparatus onto a vibration-damping or vibration-

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In the case of electromagnetic and/or magnetic interference fields, according to the prior art, these fields are detected and compensated for by means of inducing a current flow through a coil outside the apparatus. This method has the disadvantage that although the interference fields are significantly reduced, by means of negative feedback, at the location where the interfering quantity is detected, this is not necessarily the case at the "actual location of occurrence", that is to say along the electron orbits in the case of an electron scanning microscope.

This is achieved in a surprisingly simple manner by means of an apparatus according to Claim 1 and a method for operating an apparatus of this type according to Claim 23.

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The first signal which is dependent on the ambient influences and is applied to the signal input of the filter can either be output by a sensor for detecting at least one physical quantity outside the apparatus, or an output of the image processing device is connected to the calibration input of the filter, with the result that the calibration signal depends on an image analysis, for example. If a sensor is used to output the first signal, it is possible to detect electromagnetic and/or magnetic fields, air vibrations and/or body or ground vibrations. In an advantageous manner, an interfering quantity, or alternatively more than one simultaneously, can be picked up and the imaging defects caused by the interfering quantity can be compensated for by the driving of one or more control elements.

The high flexibility of the invention is also demonstrated in the fact that the effect according to the invention on the imaging and/or on the image display can take place in dependence on the interfering quantities in diverse ways. The actuators and control elements used may preferably be internal ones that are present, for example deflection systems or adjustment arrangements of sample stages. In addition to actuators which are assigned to the scanning device, it is possible, furthermore, to use, as further actuators, all systems which, like force actuators or distance drives, are sensitive to vibration, for the purpose of applying the correction signal. Furthermore, it is also possible to realize the compensation of the imaging defects by driving a control element in an image processing device, without influencing the defective imaging itself. In this case, this control element in the image processing direction comprises for example an adjustable parameter for a calculation in the image processing device. The use of multi-axis sensors and control elements advantageously enables the compensation of interference in a number of spatial directions. For this purpose, it is possible, by way of example, to vary the calibration signal at the filter as a function of the scanning location and/or of time.

In an advantageous embodiment, the apparatus, for example a microscope, is operated in a calibration mode and subsequently in an image mode, whereby, in the calibration mode, ambient influences that degrade the imaging are detected by the imaging of a predetermined reference object and comparison of the image with the real structure of the reference object, and are greatly reduced or essentially compensated for by calibration, and whereby the imaging defects are compensated for by maintaining the calibration in the imaging mode, even in the event of a change in the ambient influences.

The calibration mode is distinguished by the fact that a correlation is produced between the respective imaging defects that have been detected and the interfering influence detected by a sensor. Conversely, this means that, from an interfering influence detected by a sensor outside the apparatus, a conclusion can be drawn about the imaging defect caused by this interfering influence and this imaging defect can be compensated for. Moreover, by means of external driving of the scanning device of the apparatus, it is possible to detect a selected section of the reference object, for example along a circle, repeatedly at time intervals. In this way, time-variable imaging defects, for example caused by a building vibration, are also identified. By varying the scanning distance, for example by altering the scanning radius, it is possible, moreover, to detect location-dependent imaging defects, that is to say imaging defects which

depend on the scanning location of the exemplary scanning microscope. Consequently, the apparatus according to the invention is set up for the detection and compensation of location- and time-dependent
5 imaging defects.

In the image mode, the actual sample is then detected in its entirety by scanning, the second signal, for setting the transfer characteristic of the filter, advantageously being derived using the data
10 determined during the calibration mode as a basis.

In a further advantageous embodiment, the apparatus is set up for automatically calibrating the filter during the image mode. In contrast to the preceding embodiment, the calibration is carried out
15 during the normal image mode. Consequently, by way of example, the customary microscopic sequence is not disrupted since it is not necessary to carry out a changeover between a sample and the reference object. In addition to the advantage of requiring less time, the apparatus responds directly to what may be an
20 unnoticed change in the interfering quantity and is calibrated anew by the transfer characteristic of the filter being set, the signal applied to the calibration input of the filter being derived from an image analysis in the image processing device. By means of a
25 line-by-line image analysis, the displacement of the line centroids of successive image lines within the whole image can be determined, for example recursively, and a second signal can be calculated from this temporal displacement for the purpose of driving the
30 calibration input of the filter. The pixel displacements of the line centroid thus serve as the amplitude of the image interference. The line frequency permits an assignment of time and frequency for a
35 correlation consideration in the case of the active application of a compensation signal dependent on the

interfering quantity, that is to say in the case of the driving of an actuator and/or of a control element which have an effect on the imaging and/or the image display. If a sensor arranged outside the apparatus and
5 serving to detect an ambient influence which degrades the imaging is read in parallel with the interference amplitude determined, at the start of each line, then this enables the simultaneous pick-up of image interference and the external interfering
10 influence causing the latter. This method thus permits a direct calculation of the transfer function of the filter, which is required in order to compensate for the interference. As an alternative, fundamental assumptions may be made, for example with regard to the
15 number of poles and zeros of the transfer functions, and individual parameters, that is to say, for example, the poles and zeros, can be optimized iteratively by means of the image analysis. The line-by-line image analysis permits the filter to be set and thus the
20 ambient influences causing the imaging defects to be compensated for, up to a frequency corresponding to half the detection frequency, in accordance with the Nyquist theorem.

The image analysis may also comprise the
25 recursive determination of the displacement of the image centroid of successive images. This is appropriate for example for transmission electron microscopes or light microscopes, which use a camera system for displaying an object. By determining the
30 displacement of the image centroid in two mutually orthogonal axes, it is thus possible, by means of a corresponding correlation with the interference quantities, to rectify the image defects in two mutually perpendicular directions by the driving of
35 corresponding actuators and/or control elements. The camera systems discussed conventionally operate between

25 and 70 Hz. Although the evaluation and thus also the compensation are reduced owing to the digitization to half the image refresh rate, given a fundamental knowledge of the transfer function between interfering
5 quantity and image interference, the actual transfer function can also be determined, by extrapolation, beyond the prescribed frequency framework. This enables compensation by the application of compensation quantities even at frequencies which are higher than
10 the image frequency of the camera system used.

In a further advantageous embodiment of the invention, not only the calibration input of the filter is fed by the image processing device, but also the signal
15 input of the filter. Consequently, it is possible for the forward-connected sensor to be dispensed with and only the displacements, obtained from the image analysis, to be fed back into suitable control elements/actuators in two mutually orthogonal directions, in which case the said
20 control elements/actuators, as in all the previous advantageous embodiments, may be assigned to the scanning device and/or to the image processing device or alternatively may be further actuators.

The invention can be used in a multiplicity of imaging and/or raster-mode scanning apparatuses which
25 are suitable for the production or observation and measurement of surfaces, for example scanning electron microscopes, force microscopes, surface roughness measuring instruments, optical scanning microscopes, light microscopes, transmission electron microscopes or
30 lithography installations.

Existing installations can be equipped by simple retrofitting to give apparatuses according to the invention for compensating for ambient influences.

The invention is described below on the basis
35 of a number of exemplary embodiments with reference to the appended drawings, in which:

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Figures 1a to 1d show different embodiments of the invention in the form of block diagrams,

Figure 2 schematically illustrates a scanning microscope according to the invention,

5 Figure 3 illustrates an exemplary reference object, of the kind that can be used for the calibration mode of the microscope in Figure 2,

10 Figure 4 shows an exemplary signal S of the image acquisition device when the microscope in Figure 2, in the calibration mode, scans and acquires a reference object on a predetermined path 9 in accordance with the coordinate x at different times,

15 Figure 5 shows the exemplary correlation between the displacement of the line centroids, which is illustrated by the curve 15, and the temporally corresponding profile 14 of an interfering quantity which is detected outside the apparatus and causes the displacement of the line centroids,

20 Figures 6a to 6c show the displacement of the image centroid of three successive images,

25 Figure 7 shows the temporal profile 17 of the displacement of the centroid from Figure 6 for the x-direction, and

Figure 8 shows an exemplary embodiment of an optical microscope corresponding to the block diagram of Figure 1c.

30 Figure 1a schematically illustrates an exemplary embodiment of the imaging and/or raster-mode scanning apparatus 1 according to the invention in the form of a scanning electron microscope in a block diagram. The numeral 1 designates the apparatus without the compensation device for compensating for ambient influences which may degrade the imaging. The apparatus
35 comprises a sensor 4 outside the apparatus, this sensor

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5 Figure 1b shows a block diagram of an apparatus 1 according to the invention, in which the calibration of the filter 5 and thus the calibration of the apparatus are carried out by means of a second signal from an image processing device which is included in the image acquisition device 2 or is connected thereto.

10 Figure 2 shows an apparatus of this type with the image processing device 2 being connected to the calibration input of the filter in the case of a scanning electron microscope. The image acquisition device 7 acquires at least one pixel of the object and supplies the image processing device 2. As in the case of the first embodiment, the signal of the sensor is fed forwards to the deflection coils. A signal for
15 driving the calibration input of the filter is generated in the image processing device 2. The calibration of the filter 5 and thus of the apparatus is described below with reference to two different embodiments.

20 According to a first embodiment, the microscope is set up for operation in a calibration mode and an image mode, whereby, in the calibration mode, ambient influences that reduce the imaging quality can be detected by the imaging of a predetermined reference
25 object and comparison of the image with the real structure of the reference object, and can be essentially eliminated by calibration of the microscope, and the imaging defects are greatly reduced or essentially compensated for, even in the event of a
30 change in the ambient influences, by maintaining the calibration in the image mode. Depending on the operating mode, the input signal of the calibration input of the filter 5 either depends on the respective measured imaging defect (calibration mode) or is
35 obtained by means of the data stored during the

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calibration mode (image mode). It is possible to switch back and forth between the calibration and image modes.

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5 The electromagnetic interference field which reduces the imaging quality, by the imaging of a predetermined section of a reference object and comparison of the image with the real structure of the reference object, and to calibrate the apparatus in such a way that

10 systematic imaging defects caused by external ambient conditions and/or caused by instrumentation are essentially compensated for. According to the invention, this calibration of the microscope is carried out by setting the transfer characteristic of

15 the filter. Figure 3 illustrates how the scanning device scans a selected section of a reference object in the calibration mode, in which case, in the digital image processing device, a stored signal assigned to the reference object is compared with the image signal

20 of the reference object that is obtained from the image acquisition device, and a signal assigned to the difference is formed and is output to the calibration input of the filter.

The calibration method in the calibration mode can be described by the following steps:

- determination of a first signal, which depends on the electromagnetic interference field at the location of the sensor, by a sensor 4;
- application of the first signal to the signal input of the filter 5;
- acquisition of a selected section of a predetermined reference object by means of an image acquisition device 7 by scanning the reference object;
- 35 - comparison of the acquired image with the real structure of the reference object;

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- determination of a defect signal assigned to the difference;
- application of the second signal, derived from the defect signal, to the regulating input of the filter for defining the transfer characteristic of the said filter;
- application of the output signal of the filter 5 to the signal input of the regulating amplifier 6;
- application of the output signal of the regulating amplifier 6 to the electron beam detection coils for the purpose of correcting the reduced image quality;
- iterative calibration of the characteristic of the filter 5, in such a way that the reduction of the imaging quality is greatly reduced or essentially compensated for, by means of the following steps:
 - comparison of the corrected image with the real structure of the reference object
 - alteration of the transfer characteristic of the filter 5 in such a way that the corrected image approximates to the real structure of the reference object;
 - storage of data for generating the determined transfer function of the filter 5 for the image mode.

In one embodiment, these data for generating the determined transfer function of the filter 5 for the image mode are stored in a memory assigned to the image processing device 2. In a further embodiment, the filter 5 is set up for storing these data. While the imaging defect is being determined, the devices for compensating for the imaging defects are switched off. The microscope according to the invention is then calibrated by the method described above, that is to say the feedforward for the measurement signal of the sensor is set as a measure of the interfering quantity.

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5 The compensation quality is measured by repeated scanning of the reference object and comparison of the image with the real structure of the reference object. By determining the compensation quality in each case and correspondingly changing the transfer function of the filter, the feedforward is iteratively changed in such a way that the imaging defects of the scanning electron microscope are minimized.

10 The microscope can be calibrated with regard to location- and/or time-variable imaging defects.

For this purpose, a reference object as shown in an exemplary fashion in Figure 3 is scanned on a predetermined path in the calibration mode. The imaged reference object comprises circular gold deposits which
15 have been deposited on a substrate and are arranged in a predetermined manner. The scanning device of the microscope is driven externally, with the result that a selected section of the reference object is acquired. This path may, for example, be closed like that shown
20 by the curve 9. Individual objects 8 are situated on this closed path, to which objects the image acquisition device 2 responds and generates a signal not equal to zero. This is shown schematically and by way of example in Figure 4, which illustrates the
25 signal profile 10 acquired at a given instant t_i during the traversal of the closed curve 9. Time-dependent interference can cause time-dependent imaging defects. For this reason, in the illustration of Figure 4, the closed curve has been traversed four times at
30 intervals. The resulting four signal profiles 10 are thus also a measure of the temporal dependence of the interference. Furthermore, the traversed curve is altered by varying the radius R , whereby location-dependent imaging defects can be detected. According to
35 the invention, the time- and/or location-dependent imaging defects are determined by comparison of the

5 image in the image processing device 2 with the predetermined reference object, which is known exactly. In the example represented in Figure 4, the time-dependent imaging defect is illustrated by the curve 11.

10 The image mode is the operating mode of the inventive scanning electron microscope in which the actual sample is measured. The filter transfer characteristic determined in the calibration mode is invariant during the subsequent image mode with regard to the characteristic defined in the calibration mode. As explained above, however, it can vary with respect to time and as a function of the scanning location.

15 Assuming an essentially constant correlation between the electromagnetic interference field and the imaging defect caused by this interfering quantity, the output signal of the filter 5, after passing through the regulating amplifier 6, is applied to the electron beam deflection unit 3, with the result that image defects are essentially compensated for even in the event of a change in the ambient influences, that is to say the strength of the electromagnetic interference field.

20 In an embodiment developed further, in addition to the electromagnetic interference fields, air vibrations and/or ground vibrations are also detected by corresponding sensors, the signals that are output pass through calibratable filters which are assigned to the respective instances of interference and have adjustable transfer characteristics, and, after additional matching in the regulating amplifier 6, are applied to the deflection unit as a further control signal and/or to other actuators, with the result that the imaging defects caused by air vibrations and/or ground vibrations are also greatly reduced or essentially compensated for.

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serves as the amplitude of the image interference. The line frequency permits an assignment of time and frequency for the correlation in the case of the active compensation signal application of the feedforward signal. If the external sensor is read in parallel with the determination of this pixel displacement at the beginning of each line, a time-parallel or simultaneous detection of the image interference and of the interfering influence that causes this interference can be performed. In principle, assuming sufficient coherence, it is thus possible to directly calculate the transfer function to be set at the filter 5 in order to essentially compensate for the image interference. In an alternative embodiment, fundamental assumptions are made concerning the poles and zeros of the transfer function of the filter, and the individual parameters of the variably configured functions are optimized iteratively.

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An exemplary method for determining the centroid displacement of successive lines is briefly outlined below. On the basis of the sampling theorem, it is possible to compensate for interference frequencies which are less than half the sampling frequency. Furthermore, the method presupposes that individual objects within the image are very much larger than the line spacing and that centroid displacements perpendicular to the scanning direction in the image are small in comparison with centroid displacements parallel to the line direction. Moreover, it is assumed that the difference in the intensity $\varepsilon_n(t)$ of neighbouring lines is small, and the intensity f_{n+1} of the line $n+1$ can be written as follows:

$$f_{n+1}(t) = f_n(t) + \varepsilon_n(t).$$

If this system is then interfered with, assuming that the interference causes a temporal displacement Δ_n of

the pixels within the line, the disturbed intensity $d_n(t)$ is given by:

$$d_{n+1}(t) = t_{n+1}(t + \Delta_{n+1}) = f_n(t + \Delta_{n+1}) + \varepsilon_n(t + \Delta_{n+1}) \text{ and} \\ d_{n+1}(t) = d_n(t + \Delta_{n+1} - \Delta_n) + \varepsilon_n(t + \Delta_{n+1}).$$

5 Using a non-causal Wiener filter, it is possible to calculate a δ pulse as a function of the line displacements Δ_{n+1} and Δ_n :

$$\delta(t + \Delta_{n+1} - \Delta_n) \approx \text{FFT}^{-1} \{ D_{n+1}(\omega) D_n^*(\omega) / |D_n(\omega)|^2 + \delta^2 \varepsilon \},$$

10 where $D_n(\omega)$ is the Fourier transform of the disturbed intensity $d_n(t)$. This δ function depends on the difference between the centroid displacement of neighbouring lines. Consequently, the centroid displacement within the lines of an image can be calculated recursively, since, as explained above
15 $(\Delta_{n+1} - \Delta_n)$ is known as a result of the image analysis. For the driving of the deflection unit of the microscope, a signal which is proportional to the correlation function of the measured interfering quantity and the calculated centroid displacements in
20 the individual lines is generated using a vector correlation. This correlation is carried out in the digital filter, a second signal, which is dependent on the temporal displacement calculated, being applied to the calibration input of the filter.

25 A further embodiment of the invention is suitable for example for transmission electron microscopes (TEM) or light microscopes or related types of apparatuses which use a camera system 20 to display the object. In the embodiment described below, the
30 apparatus illustrated in the block diagram in Figure 1c corresponds to the optical microscope 18 illustrated in Figure 8. The external sensor 4 is designed as a multi-axis vibration sensor whose signal is passed via an adjustable filter 5 and an amplifier 6 to a control
35 element, which, in the present embodiment, is assigned directly to the imaging processing device 21 and has an

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effect on the image in the latter. In Figure 8, the filter, the amplifier and the control element are not explicitly shown but rather are contained integrally in the image processing device 21. According to the invention, then, in this apparatus a compensation signal is not applied to an actuator which influences the imaging, rather, instead of this, the image display is influenced directly. The camera system comprises a CCD camera 19 with a monitor, an image frequency of 25 Hz being worked with. The image processing device 21 is set up for storing successive images. By means of image analysis, the displacement of the image centroid of successive images in two mutually orthogonal directions is calculated and used to set the transfer function of the digital filter 5 in a similar manner to that in the embodiment described above. An illustrative representation of this displacement of the centroid of successive images is shown in Figures 6 and 7. The curve 17 in Figure 7 shows the profile of the coordinate x of the centroid with time. The differences between two scanning points, for example t_0 and t_1 , thus correspond to the image refresh frequency.

A further embodiment, in comparison with the embodiment described above, enables instances of interference to be corrected by the compensation signal application even at frequencies which are greater than the image refresh frequency of 25 Hz. For this purpose, the transfer function, which is defined by the points of resonance in the mechanical construction of the microscope, is implemented as the filter 5. In this way, a base vibration X generates a relative movement Δx at the microscope. The general transfer function is thus completely determined by the actual sensitivity $\Delta x/X$, the resonant frequency f_R and by the parameter Q, which defines the asymptotic decline of $\Delta x/X$ at high frequencies. By determining three points on the curve

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below the resonant frequency f_R as well, it is thus possible to infer the entire function and use it in the feedforward control by application of a compensation signal also for interference frequencies which are greater than the image refresh frequency.

In contrast to the embodiments described heretofore, according to the invention it is possible, moreover, to use the image information not in a feedforward arrangement but in a traditional feedback arrangement for the compensation of image interference. This is illustrated schematically in the block diagram 1d. The sensor whose signal is fed forwards is omitted, and instead of this the centroid displacements determined in the x- and/or y- axis from the image analysis are fed back into a suitable control element, in this case a device for displacing the sample, after passing through an adjustable transfer function.

In further embodiments (not illustrated in any detail here) of the invention, the apparatus may be a force microscope, a surface roughness measuring instrument, an optical scanning microscope or a lithography installation.

Depending on the embodiment, in the case of electron microscopes, the driven actuators and control elements comprise the already described electron beam deflection devices and/or control elements in the image processing device, and in the case of optically operating apparatuses, the actuators comprise, depending on the embodiment, devices for deflecting the light and/or devices for deflecting the sample and/or control elements in the image processing device. A control element in the image processing device in this case designates, by way of example, the influence on a parameter which has effects on the calculation of the image. Moreover, use is made of further actuators which are sensitive to vibrations, and also force actuators

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(electrodynamic linear drives) and distance drives (piezotranslators).

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